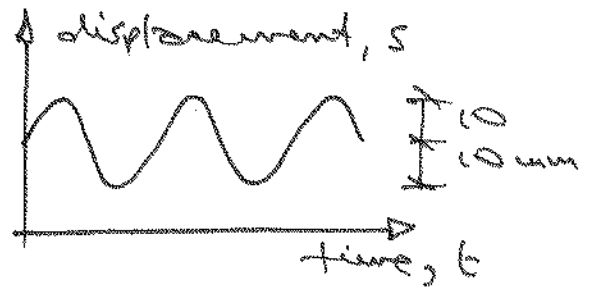


Displacement  $s$  of mass  $m$   
 $s = \bar{s} + r \sin \omega t$ ;  $r = 10 \text{ mm}$   
 $\therefore \ddot{s} = \omega^2 r$  and so  
 maximum force which  
 has to be exerted by  
 return spring is follows



$$F_{\text{coll.}} = m \omega^2 r$$

$$= 9 \frac{\text{kg}}{\text{m}^3} (2\pi \times 10)^2 \times 0.01 = \frac{355}{2} \text{ N}$$

We'd choose a larger value  
 say 450 N so that we've got  
 a safety factor dynamically.

Select  $F_{10} = \frac{1}{3} F_{\text{lim}}$ , which  
 results in desired characteristic:-

$$k = 300/20 = 15 \text{ N/mm}$$

Assume a strength safety factor of 1.1

trial c say

Using the fatigue expression (5b) for unwin  
 wire, e.g. with  $c = 5$ :

$$F_e = 600(s+0.5)/0.50 + 300 \times 5 \frac{5.6}{4.73}/0.15$$

which gives  $F_e$  (kN)      19.5      27.4      35.3

hence min.  $F_{ut} = 1.1 F_e$       21.5      30.1      38.8

So, from Table, necessary  $d$ :      4      5      ?? > 5

Actual  $n$ :

$$n = Gd / 8kC^3$$

(note large  $n$  w/ small  $C$ )

$n_T$  Table 1 (ends 5+6)      23      9 <sup>3/4</sup>

$L_s = n_T d$  (mm)      52      48.8

$\delta_s = \text{say } 1.1 \delta_{\text{lim}}$       33      33

$l_0 = L_s + \delta_s$  (mm)      125      82

BUCKLING. say ends guided  $\lambda = 0.5$

$\lambda l_0 / c_2 D$       1.19      0.42 < 1

$\delta_c$  (32) (mm)      46 >  $\delta$       no buckling possible

OK,      OK

RESONANCE TENDENCY. from (6)

$f_n$  (Hz)      170      164

$f_n / f_{\text{exciting}}$       12 < 17.0      16.4 > 12

OK      OK

Both trial solutions are feasible, as will  
 be intermediate candidates. Further evaluation  
 would be based on cost, space saving &c.