

1. The basic equation for equivalent load is

$$P_e^n \Delta t = \int_0^t P^n dt$$

where, for a triangular waveform

$$\therefore \int_0^t P^n dt = (\hat{P}/\delta t)^n \int_0^t t^n dt = \frac{\hat{P}^n}{n+1} \delta t$$

Applying this to the given cycle :-

$$P_e^n \cdot 60 = \frac{1}{n+1} (7.5^n \times 10 + 1.5^n \times 50) \text{ whence}$$

$$\text{for } n=2 \quad P_e = 1.94 \text{ kW}$$

$$n=5 \quad P_e = 3.66 \text{ kW}$$

Note that power has been used here, rather than torque, since essentially at constant speed.

(a) For P_e of 1.94 kW, a 100 LA motor is indicated.

Check on peak torque at $n_f = 1430 \text{ rpm}$

$$\hat{T} = 7.5 \times 10^3 / \frac{1430}{60} \times 2\pi = 50.1 \text{ Nm}$$

Whereas the breakdown torque of this motor is

$$T_b = 15.0 \times 3.2 = 48.0 \text{ Nm}$$

i.e. motor is unsuitable since $T_b < \hat{T}_{load}$

Trying larger motors, the smallest such $T_b > \hat{T}$ is 150 LB, with $T_b = 20.0 \times 3.3 = 66 \text{ Nm}$.

So select 150 LB, though even with this, the peak torque is rather excessive.

(b) For $P_e = 3.66 \text{ kW}$, try 112 M motor ($P_f = 4.0 \text{ kW}$)

$$T_b = 27.0 \times 3.3 = 89.1 \text{ Nm} > \hat{T} - \text{OK.}$$

With a cycle time of 1 minute, the number of starts per hour is relevant. However load increases gradually rather than square wave, so ignore here. Also don't know load inertia.

A flywheel might profitably be considered here to reduce the peak torque seen by the motor.

2. There are two aspects to consider - intermittency and frequency of starts.

Let the cyclic duration factor be γ

From the basic relation

$$T_e^n \cdot \Delta t = \int_0^t T dt = (T^n \gamma \Delta t + 0)$$

$$T_e = T \cdot \gamma^{1/n}$$

$$\text{with } n=6, \quad T_e = 25 \times \left(\frac{20}{40}\right)^{1/6} = 21.8 \text{ Nm}$$

Alternatively using $n=16/3$, $T_e = 22.0 \text{ Nm}$. - which approximates manufacturers' recommendation.

So a 112 M motor is indicated ($T_f = 27 \text{ Nm}$).

Now check for frequency of starts.

