

Height of load over datum =  $l \cos \theta$

$$\therefore \text{P.E. gain} = P \cdot l (\cos \theta - \cos \theta_0).$$

$$\text{Deflection of a spring} = \frac{k}{2} (\sin \theta - \sin \theta_0)$$

$$\therefore \text{SE. gain of both springs} = 2 \cdot \frac{l}{2} k \cdot \frac{k^2}{2} (\sin \theta - \sin \theta_0)^2$$

$$\text{Total energy} = \frac{1}{2} k l^2 (\sin \theta - \sin \theta_0)^2 + P l (\cos \theta - \cos \theta_0)$$

$$\text{Set } V = \text{energy} / \frac{1}{2} k l^2 \text{ & set } p = 2P/kl$$

$$= \frac{1}{2} (\sin \theta - \sin \theta_0)^2 + p (\cos \theta - \cos \theta_0).$$

$$\textcircled{1} \quad V' = (\sin \theta - \sin \theta_0) \cos \theta - p \sin \theta$$

$$\textcircled{2} \quad V'' = \cos 2\theta + \sin \theta \sin \theta - p \cos \theta$$

PERFECT  $\theta_0 = 0$  - critical buckling at  $p_c$ .

$$V' = \sin \theta (\cos \theta - p) \quad \text{from } \textcircled{1}.$$

$$V'' = \cos 2\theta - p \cos \theta \quad \text{from } \textcircled{2}.$$

$$V' = 0 \quad \text{for equilibrium, } \infty$$

- $$\textcircled{3} \quad \text{either } \sin \theta = 0, \theta = 0 \quad \text{in which case } V'' = 1 - p \\ \text{neutral } V'' = 0, p = 1 \quad \text{this is unstable, i.e. } p_c = 1 \\ \text{stable } V'' > 0, p < 1 \quad \text{i.e. } p < p_c \\ \text{unstable } V'' < 0, p > 1 \quad \text{i.e. } p > p_c$$

$$\text{Critical load } p_c = \frac{1}{2} k l,$$

- $$\textcircled{4} \quad \text{or } p = \cos \theta \quad \text{in which case } V'' = -\sin^2 \theta. \\ \text{i.e. this is unstable } (V'' < 0) \text{ for all } \theta.$$

There are therefore three post-buckling paths, all of which are unstable -  $\theta = 0^\circ$  and  $\theta = \cos^{-1} p$  ( $\theta$  is positive or negative).

IMPERFECT  $|\theta| > |\theta_0| > 0$  - no critical but possible  $\hat{p}$ .

$$V' = 0 \quad \text{for equilibrium, } \infty, \text{ from } \textcircled{1}:$$

$$\textcircled{5} \quad p = (1 - \sin \theta_0 / \sin \theta) \cos \theta$$

Note that, mathematically,  $p > 0$  for all  $|\theta| > |\theta_0|$ .

Inserting  $\textcircled{5}$  into  $\textcircled{2}$ :

$$\textcircled{6} \quad V'' = (\sin \theta - \sin^3 \theta) / \sin \theta \quad \text{for the semi-circle trajectory.}$$

Maximum  $p = \text{re. } \hat{p}$  - will occur when  $p' = 0$  i.e. when  $V'' = 0$  - that is when equilibrium is neutral. In this case, from  $\textcircled{6}$   $\sin^3 \theta = \sin \theta_0$ , so that, from  $\textcircled{5}$ :

$$\textcircled{7} \quad \hat{p}' = [1 - (\sin \theta_0)^{2/3}]^{3/2},$$

- which is superimposed on the trajectory's overtangency.

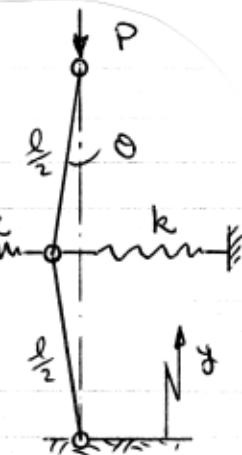
Considering positive  $\theta, \theta_0$ , from  $\textcircled{6}$ :

$$\sin^3 \theta < \sin \theta_0, V'' > 0, \text{ stable.}$$

$$\sin^3 \theta > \sin \theta_0, V'' < 0, \text{ unstable.}$$

which are exemplified in the trajectories' slopes.

Note that the trajectories are shown also for negative  $p$  corresponding to a tensile force necessary for  $|\theta| < |\theta_0|$



cont'd. . .