

First derive expression for availability of pivoted shoe given μ and the geometry - r , e , b_x , b_y and the vectors of lining integrals \vec{J}_S and \vec{J}_C .

For simplicity, define $\zeta = \Delta d/\mu$ & let $' \equiv d/d\zeta$

$$(a) \begin{cases} \alpha = [\zeta e \ 0 \ -\zeta r] & \alpha' = [\zeta \ 0 \ -r] \\ \beta = [(\zeta b_x - b_y)(\zeta b_y + b_x) - \zeta r] & \beta' = [b_x \ b_y \ -r] \end{cases}$$

Define also the ratio ν between lining press. components

$$(b) \quad \nu \equiv N_c/N_s = r_c/r_s \quad \Delta = -\beta J_S / \beta J_C \quad \text{from (1)}$$

and form the vector \vec{J}_0 viz:

$$(c) \quad \vec{J}_0 = \vec{J}_S + \nu \vec{J}_C$$

-noting that $\alpha, \alpha', \beta, \beta', \nu, \vec{J}_0$ are all computable given the known geometry, so is:

$$(d) \quad \nu' = -\frac{d}{d\zeta} (\beta J_S / \beta J_C) = -(\beta' J_S / \beta J_C - \beta J_S \cdot \beta' J_C / (\beta J_C)^2) \\ = -(\beta' J_S + \nu \beta' J_C) / \beta J_C = -\beta' \vec{J}_0 / \beta J_C$$

In this \vec{J}_0 notation, equations (5c) & (7c) take the form:-

$$(e) \quad \begin{bmatrix} F_x \\ F_y \end{bmatrix} = N_s \begin{bmatrix} \Delta & -d\mu \\ d\mu & \Delta \end{bmatrix} \begin{bmatrix} I_{Sc} + \nu I_{Cc} \\ I_{Ss} + \nu I_{Sc} \end{bmatrix} = N_s \begin{bmatrix} \Delta & -d\mu \\ d\mu & \Delta \end{bmatrix} \begin{bmatrix} \vec{J}_0(1) \\ \vec{J}_0(2) \end{bmatrix}$$

$$(f) \quad |T| = \mu r N_s (I_S + \nu I_C) = N_s \mu r \vec{J}_0(3)$$

$$(g) \quad M = N_s \alpha (\vec{J}_S + \nu \vec{J}_C) = N_s \cdot \alpha \vec{J}_0$$

The mechanical advantage, η is

$$\eta = |T|/M = \mu r \vec{J}_0(3) / \alpha \vec{J}_0$$

$$d\eta/d\mu = r \left\{ \vec{J}_0(3) / \alpha \vec{J}_0 + \zeta \left((\vec{J}_0(3))' / \alpha \vec{J}_0 - \vec{J}_0(3) (\alpha \vec{J}_0)' / (\alpha \vec{J}_0)^2 \right) \right\} \\ = \frac{\eta}{\mu} \left(1 + \zeta \left(\frac{(\vec{J}_0(3))'}{\vec{J}_0(3)} - \frac{(\alpha \vec{J}_0)'}{\alpha \vec{J}_0} \right) \right)$$

-and as the availability, from (vii) is:

$$(h) \quad S = 1 + \zeta \left((\vec{J}_0(3))' / \vec{J}_0(3) - (\alpha \vec{J}_0)' / \alpha \vec{J}_0 \right)$$

in which

$$(m) \quad (\vec{J}_0(3))' = \frac{d}{d\zeta} (I_S + \nu I_C) = \nu' I_C = \nu' \vec{J}_C(3)$$

$$(n) \quad (\alpha \vec{J}_0)' = \frac{d}{d\zeta} (\alpha \vec{J}_0) = \alpha' \vec{J}_0 + \alpha \vec{J}_0' \\ = \alpha' \vec{J}_0 + \alpha (I_S + \nu I_C) = \alpha' \vec{J}_0 + \nu' \alpha \vec{J}_C$$

All terms herein have been defined, hence S.

Calculating parameters for the LH shoe, $\Delta d = 1$, $\zeta = 0.3$ given geometry:

$$r = 10'' \quad e = 12.37'' \quad b_x = 11 \cos 80^\circ = 1.91'' \quad b_y = 11 \sin 80^\circ = 10.93''$$

$$\therefore \text{from (a)} \quad \alpha = [3.71 \ 12.37 \ -3] \text{ in}, \quad \alpha' = [12.37 \ 0 \ -10] \text{ in} \\ \beta = [-10.26 \ 5.16 \ -3] \text{ in}, \quad \beta' = [1.91 \ 10.93 \ -10] \text{ in}$$

and the integral vectors :-

$$\vec{J}_S = [0.236 \ 1.436 \ 1.714] \quad \vec{J}_C = [0.933 \ 0.236 \ 0.590]$$

Applying (b):

$$\beta J_C = [-10.26 \ 5.16 \ -3][0.933 \ 0.236 \ 0.590] = -9.096 \\ \beta J_S = [-10.26 \ 5.16 \ -3][0.236 \ 1.436 \ 1.714] = -0.150 \quad \nu = \frac{-0.0165}{-9.096}$$

$$\therefore \text{from (c)} \quad \vec{J}_0 = \begin{bmatrix} 0.236 - 0.0165 \times 0.933 \\ 1.436 - 0.0165 \times 0.236 \\ 1.714 - 0.0165 \times 0.590 \end{bmatrix} = \begin{bmatrix} 0.222 \\ 1.432 \\ 1.704 \end{bmatrix}$$